

中尺度扰动的对称发展*

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提 要

本文主要研究了斜压基本气流中中尺度对称型扰动发展的问题,旨在揭示中尺度扰动发展的内在本质。文中应用 WKB 方法,分析了二维动量无辐散近似下的扰动方程。结果是,中尺度扰动波包对称发展的原因是基本场的不均匀热成风偏差和非定常性。

一、引 言

强对流活动往往表现为组织化的中尺度系统,如飑线, MCC 等。这种组织化的中尺度系统形成于一定的背景条件之下,它们无论在启动和组织更小尺度的对流方面,还是在 大、中、小尺度天气系统之间的相互反馈和作用方面都起着关键的作用。因此,从物理本质方面彻底弄清楚这些中系统形成的原因是十分重要的。本文基于这一点,着重讨论了弱热成风平衡的大尺度背景下,中尺度扰动对称发展的原因及其与大尺度背景场的相互作用问题,揭示了一些内在的规律。

数十年来,中尺度动力学的研究已经有了长足的进步。尤其是准地转基流下,非地转平行型扰动的稳定性问题更是可喜。Kuo^[1]讨论过对称不稳定;Ooyama^[2]用对称不稳定讨论过台风轴对称扰动。Hoskins^[3,4], Emanuel^[5]及 Ogura 等^[6]发现了中尺度对称不稳定性扰动可能在组织和启动带状对流活动方面有重要作用。最近 Kuo 和 Seitter^[7]还讨论了中性及部分不稳定大气中切变地转流的稳定性;张可苏^[8]讨论了有界域中的对称不稳定性问题。这些研究丰富了我们关于中尺度扰动稳定性方面的知识。本文与上述工作不同。本文应用了 WKB 方法,从能量学的整体角度研究一个扰动波包的发展、演变,获得了有益的结果。

二、基本方程组

张可苏^[9]曾在“大气动力学模式的比较研究”中指出,适合于中尺度运动的方程组是准动量无辐散模式。在 f -平面内,斜压层结流中小扰动的准动量无辐散模式可以写成(不考虑声波):

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$$\begin{cases} \left(\frac{\partial}{\partial t} + \bar{u} \frac{\partial}{\partial x}\right)u + w\bar{u}_z - f_a v + \frac{\partial p'}{\partial x} = 0 \\ \left(\frac{\partial}{\partial t} + \bar{u} \frac{\partial}{\partial x}\right)v + f u + \frac{\partial p'}{\partial y} = 0 \\ \left(\frac{\partial}{\partial t} + \bar{u} \frac{\partial}{\partial x}\right)w + \frac{\partial p'}{\partial z} - \theta = 0 \\ \left(\frac{\partial}{\partial t} + \bar{u} \frac{\partial}{\partial x}\right)\theta - M^2 v + N^2 w = Q \\ \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0 \end{cases} \quad (1)$$

其中, $(u, v, w, \theta) \equiv \bar{\rho} \left(u', v', w', \frac{g}{\theta} \theta' \right)$

$$M^2 = -\frac{g}{\theta} \frac{\partial \bar{\theta}}{\partial y}$$

$$N^2 = \frac{g}{\theta} \frac{\partial \bar{\theta}}{\partial z}$$

$$Q = \frac{\bar{\rho} g}{c_p T} \dot{H}$$

$$f_a = f - \bar{u}_y$$

这里“—”表示基本场;“'”代表扰动场; $\bar{\rho} \dot{H}$ 表示单位体积加热率; $\bar{u}(y, z)$ 表示基本场风速; f_a 为基本场绝对涡度, $\bar{\theta}$ 为基本场位温。

为了数学处理方便,我们考虑扰动是对称型发展的情况,即可设 $\frac{\partial F}{\partial x} = 0$, F 为任意变量。那么,在 (y, z) 平面中利用连续方程引入质量流函数 ψ

$$\begin{cases} v = \frac{\partial \psi}{\partial z} \\ w = -\frac{\partial \psi}{\partial y} \end{cases} \quad (2)$$

则方程组(1)可改写成:

$$\begin{cases} \frac{\partial}{\partial t} \nabla^2 \psi = -f \frac{\partial u}{\partial z} - \frac{\partial \theta}{\partial y} \\ \frac{\partial u}{\partial t} = f_a \frac{\partial \psi}{\partial z} + \bar{u}_z \frac{\partial \psi}{\partial y} \\ \frac{\partial \theta}{\partial t} = M^2 \frac{\partial \psi}{\partial z} + N^2 \frac{\partial \psi}{\partial y} \end{cases} \quad (3)$$

在(3)式中已假定 $Q \equiv 0$, 即不考虑热源影响。从(3)式中消去变量 u 和 θ , 则得到关于流函数 $\psi(y, z)$ 的单一方程。

$$\begin{aligned} & \nabla^2 \psi_{tt} + f f_a \psi_{zz} + (f \bar{u}_z + M^2) \psi_{yz} + N^2 \psi_{yy} \\ & + \left(\frac{\partial}{\partial z} f f_a + \frac{\partial M^2}{\partial y} \right) \frac{\partial \psi}{\partial z} + \left(\frac{\partial f \bar{u}_z}{\partial z} + \frac{\partial N^2}{\partial y} \right) \frac{\partial \psi}{\partial y} = 0 \end{aligned} \quad (4)$$

Ooyama 和 Hoskins 以及张可苏等都在热成风平衡假定下讨论过这个方程的特征值问题。

本文将应用 WKB 方法研究非热成风平衡假定下的完整方程(4)式。

三、波群分析

先引入“伸长”坐标 $Y = \varepsilon y, Z = \varepsilon z$, 和“延迟”时间 $T = \varepsilon t$, 并假定质量流函数具有波包形式^[10,11],

$$\psi = A e^{i\theta} \quad (5)$$

其中,

$$A = A(Y, Z, T) = A_0(Y, Z, T) + \varepsilon A_1(Y, Z, T) + \dots \quad (6)$$

$$\theta = kY + nZ - \omega T \quad (7)$$

ε 为小参数

将(5)、(6)、(7)代入(4)式,并按小参数 ε 的幂次整理,则得:

$$\varepsilon^0: \omega^2 \gamma^2 = n^2 f f_a + nk(f\bar{u}_z + M^2) + k^2 N^2 \quad (8)$$

$$\begin{aligned} \varepsilon^1: & 2\omega \frac{\partial}{\partial T} (\gamma^2 A_0) + \frac{\partial A_0}{\partial Y} [-2\omega^2 k + n(f\bar{u}_z + M^2) + 2kN^2] \\ & + \frac{\partial A_0}{\partial Z} [-2\omega^2 n + k(f\bar{u}_z + M^2) + 2nff_a] + \gamma^2 \frac{\partial \omega}{\partial T} A_0 \\ & - \omega^2 A_0 \left(\frac{\partial k}{\partial Y} + \frac{\partial n}{\partial Z} \right) + ff_a \frac{\partial n}{\partial Z} A_0 + (f\bar{u}_z + M^2) \frac{\partial n}{\partial Y} A_0 \\ & + N^2 \frac{\partial k}{\partial Y} A_0 + \left(\frac{\partial ff_a}{\partial Z} + \frac{\partial M^2}{\partial Y} \right) n A_0 + \left(\frac{\partial f\bar{u}_z}{\partial Z} + \frac{\partial N^2}{\partial Y} \right) k A_0 = 0 \end{aligned} \quad (9)$$

其中 $\gamma^2 = k^2 + n^2$

方程(8)即为频散关系式,方程(9)式则为振幅方程式。

应用频散关系式(8),可以得到群速度

$$C_{\varepsilon r} = \frac{\partial \omega}{\partial k} = \frac{\gamma^{-2}}{2\omega} [-2\omega^2 k + n(f\bar{u}_z + M^2) + 2kN^2] \quad (10)$$

$$C_{\varepsilon z} = \frac{\partial \omega}{\partial n} = \frac{\gamma^{-2}}{2\omega} [-2\omega^2 n + k(f\bar{u}_z + M^2) + 2nff_a] \quad (11)$$

记

$$\frac{d_{\varepsilon}}{dt} = \frac{\partial}{\partial T} + C_{\varepsilon r} \frac{\partial}{\partial Y} + C_{\varepsilon z} \frac{\partial}{\partial Z} \quad (12)$$

则利用(8)式还可以求得扰动的波参数变化方程:

$$\frac{d_{\varepsilon} k}{dT} = -\frac{\gamma^{-2}}{2\omega} \left(n^2 \frac{\partial ff_a}{\partial Y} + nk \frac{\partial (f\bar{u}_z + M^2)}{\partial Y} + k^2 \frac{\partial N^2}{\partial Y} \right) \quad (13)$$

$$\frac{d_{\varepsilon} n}{dT} = -\frac{\gamma^{-2}}{2\omega} \left(n^2 \frac{\partial ff_a}{\partial Z} + nk \frac{\partial (f\bar{u}_z + M^2)}{\partial Z} + k^2 \frac{\partial N^2}{\partial Z} \right) \quad (14)$$

$$\frac{d_{\varepsilon} \gamma^2}{dT} = -\frac{\gamma^{-2}}{\omega} \left(n^2 \frac{\partial ff_a}{\partial l_0} + nk \frac{\partial (f\bar{u}_z + M^2)}{\partial l_0} + k^2 \frac{\partial N^2}{\partial l_0} \right) \quad (15)$$

$$\frac{d_{\varepsilon} (k/n)}{dT} = -\frac{\gamma^{-2}}{2\omega n^2} \left(n^2 \frac{\partial ff_a}{\partial l_{\perp}^0} + nk \frac{\partial (f\bar{u}_z + M^2)}{\partial l_{\perp}^0} + k^2 \frac{\partial N^2}{\partial l_{\perp}^0} \right) \quad (16)$$

其中 $l_0 = \gamma^{-2}(Ry + nk)$, $l_{\perp}^0 = \gamma^{-2}(nj - k\mathbf{k})$ 将(10)和(11)式代入(9)式,并在方程两边

乘上 A_0 则得能量方程:

$$\begin{aligned} & \frac{\partial}{\partial T}(\gamma^2 A_0^2) + \nabla \cdot (\gamma^2 A_0^2 \mathbf{C}_e) - \frac{A_0^2}{\omega} \omega \nabla \cdot (\gamma^2 \mathbf{C}_e) \\ & + \frac{A_0^2}{\omega} \left[\gamma^2 \frac{\partial \omega}{\partial T} + \omega \frac{\partial \gamma^2}{\partial T} - \omega^2 \left(\frac{\partial k}{\partial Y} + \frac{\partial n}{\partial Z} \right) + f f_a \frac{\partial n}{\partial Z} \right. \\ & + (f \bar{u}_z + M^2) \frac{\partial n}{\partial Y} + N^2 \frac{\partial k}{\partial Y} + \left(\frac{\partial f f_a}{\partial Z} + \frac{\partial M^2}{\partial Y} \right) n \\ & \left. + \left(\frac{\partial f \bar{u}_z}{\partial Z} + \frac{\partial N^2}{\partial Y} \right) k \right] = 0 \end{aligned} \quad (17)$$

利用(10)和(11)式可得

$$\begin{aligned} \omega \nabla \cdot (\gamma^2 \mathbf{C}_e) = & -\omega \left[\omega \left(\frac{\partial k}{\partial Y} + \frac{\partial n}{\partial Z} \right) + k \frac{\partial \omega}{\partial Y} + n \frac{\partial \omega}{\partial Z} \right] \\ & + \omega \left[\frac{\partial k}{\partial Y} \frac{N^2}{\omega} - \frac{k N^2}{\omega^2} \frac{\partial \omega}{\partial Y} + \frac{k}{\omega} \frac{\partial N^2}{\partial Y} \right] \\ & + \omega \left[\frac{f f_a}{\omega} \frac{\partial n}{\partial Z} - \frac{n f f_a}{\omega^2} \frac{\partial \omega}{\partial Z} + \frac{n}{\omega} \frac{\partial f f_a}{\partial Z} \right] \\ & + \omega \left[\frac{1}{2\omega} (f \bar{u}_z + M^2) \left(\frac{\partial n}{\partial Y} + \frac{\partial k}{\partial Z} \right) - \frac{(f \bar{u}_z + M^2)}{2\omega^2} \left(n \frac{\partial \omega}{\partial Y} + k \frac{\partial \omega}{\partial Z} \right) \right] \\ & + \frac{\omega}{2\omega} \left[n \frac{\partial (f \bar{u}_z + M^2)}{\partial Y} + k \frac{\partial (f \bar{u}_z + M^2)}{\partial Z} \right] \end{aligned} \quad (18)$$

由(8)式可得

$$\begin{aligned} \gamma^2 \frac{\partial \omega}{\partial T} = & -\frac{\omega^2}{2\omega} \frac{\partial \gamma^2}{\partial T} + \frac{2n f f_a}{2\omega} \left(-\frac{\partial \omega}{\partial Z} \right) - \frac{\left(k \frac{\partial \omega}{\partial Z} + n \frac{\partial \omega}{\partial Y} \right)}{2\omega} (f \bar{u}_z + M^2) \\ & + \frac{2k}{2\omega} \left(-\frac{\partial \omega}{\partial Y} \right) N^2 + \frac{1}{2\omega} \left(\frac{\partial f f_a}{\partial T} n^2 + n k \frac{\partial}{\partial T} (f \bar{u}_z + M^2) + k^2 \frac{\partial N^2}{\partial T} \right) \end{aligned} \quad (19)$$

将(18)、(19)式代入(17)式,并注意到 $\gamma^2 = k^2 + n^2$ 和

$$\frac{\partial \omega}{\partial Y} = -\frac{\partial k}{\partial T}, \quad \frac{\partial \omega}{\partial Z} = -\frac{\partial n}{\partial T}, \quad \frac{\partial n}{\partial Y} = \frac{\partial k}{\partial Z} \quad (20)$$

则(17)式可以写成

$$\begin{aligned} & \frac{\partial}{\partial T}(\gamma^2 A_0^2) + \nabla \cdot (\gamma^2 A_0^2 \mathbf{C}_e) + \frac{A_0^2}{2\omega} \left[n \left(\frac{\partial f f_a}{\partial Z} + \frac{\partial M^2}{\partial Y} \right) \right. \\ & + k \left(\frac{\partial f \bar{u}_z}{\partial Z} + \frac{\partial N^2}{\partial Y} \right) \left. + \frac{A_0^2}{2\omega^2} \left[k^2 \frac{\partial N^2}{\partial T} + n k \frac{\partial}{\partial T} (f \bar{u}_z + M^2) \right. \right. \\ & \left. \left. + n^2 \frac{\partial f f_a}{\partial T} \right] \right] = 0 \end{aligned} \quad (21)$$

在整个波包区域中积分(21)式,并假定波包的边缘上扰动的振幅 $A_0 = 0$,则获得扰动波包的能量方程如下:

$$\frac{\partial}{\partial T} \iint_{\sigma} (\gamma^2 A_0^2) dY dZ = - \iint_{\sigma} \frac{A_0^2}{2\omega} \left[n \left(\frac{\partial f f_a}{\partial Z} + \frac{\partial M^2}{\partial Y} \right) \right.$$

$$+ k \left(\frac{\partial f \bar{u}_z}{\partial Z} + \frac{\partial N^2}{\partial Y} \right) dY dZ - \iint_{\sigma} \frac{A_0^2}{2\omega^2} \left[k^2 \frac{\partial N^2}{\partial T} + nk \frac{\partial (f \bar{u}_z + M^2)}{\partial T} + n^2 \frac{\partial f f_a}{\partial T} \right] dY dZ \quad (22)$$

其中下标 σ 表示整个波包区域。

四、扰动波包对称发展的分析

由于扰动波包的能量为 $\iint_{\sigma} \gamma^2 A_0^2 dY dZ$, 所以可以定义对称发展, 即 (Y, Z) 平面内重力惯性波波包发展的条件为:

$$\frac{\partial E}{\partial T} = \frac{\partial}{\partial T} \iint_{\sigma} \gamma^2 A_0^2 dY dZ \begin{cases} > 0 & \text{对称发展} \\ < 0 & \text{对称衰减} \end{cases} \quad (23)$$

1. 如果基本场满足热成风平衡, 则

$$M^2 = -g \frac{\partial \ln \bar{\theta}}{\partial y} = f \bar{u}_z = f \bar{u}_\sigma \quad (24)$$

于是

$$\frac{\partial f f_a}{\partial Z} = \frac{\partial}{\partial Z} f(f - \bar{u}_z) = -f \frac{\partial \bar{u}_z}{\partial Y} = -\frac{\partial M^2}{\partial Y} \quad (25)$$

$$\frac{\partial f \bar{u}_z}{\partial Z} - \frac{\partial M^2}{\partial Z} = -g \frac{\partial^2 \ln \bar{\theta}}{\partial Z \partial y} = -\frac{\partial N^2}{\partial Y} \quad (26)$$

将(25)、(26)式代入(22)式中便得

$$\frac{\partial}{\partial T} \iint_{\sigma} \gamma^2 A_0^2 dY dZ = - \iint_{\sigma} \frac{A_0^2}{2\omega^2} \left[k^2 \frac{\partial N^2}{\partial T} + 2nk \frac{\partial M^2}{\partial T} + n^2 \frac{\partial f f_a}{\partial T} \right] dY dZ \quad (27)$$

这样我们便得到如下的能量守恒定理:

如果大尺度基本场是定常的且热成风平衡的, 则对称扰动波包能量守恒。此时扰动波包不发展, 也不衰减。

2. 如果基本场是热成风平衡的, 但不定常, 则扰动波包对称发展必须满足:

$$k^2 \frac{\partial N^2}{\partial T} + 2nk \frac{\partial M^2}{\partial T} + n^2 \frac{\partial f f_a}{\partial T} < 0 \quad (28)$$

若 $\frac{\partial N^2}{\partial T} > 0$, 则此式可以写成:

$$\left(k + n \frac{\partial M^2 / \partial T}{\partial N^2 / \partial T} \right)^2 + \left[\frac{\partial f f_a / \partial T}{\partial N^2 / \partial T} - \left(\frac{\partial M^2 / \partial T}{\partial N^2 / \partial T} \right)^2 \right] n^2 < 0$$

由此可得出在 $\frac{\partial N^2}{\partial T} > 0$ 时扰动波包对称发展的必要条件为

$$\left(\frac{\partial M^2}{\partial T} \right)^2 - \frac{\partial f f_a}{\partial T} \cdot \frac{\partial N^2}{\partial T} > 0 \quad (29)$$

同理, 若 $\frac{\partial N^2}{\partial T} < 0$ 时, 可得到扰动波包对称发展的充分条件为

$$\left(\frac{\partial M^2}{\partial T}\right)^2 - \frac{\partial f f_a}{\partial T} \frac{\partial N^2}{\partial T} < 0 \quad (30)$$

3. 如果基本场定常, 但不满足热成风平衡条件, 即存在热成风偏差, 则扰动波包可能会对称发展。

若记 $M^2 = -g \frac{\partial \ln \bar{\theta}}{\partial y} \equiv f \bar{u}_\theta, \bar{u}_\theta$ 为热成风, 而记 $\Delta \bar{u}_\theta = \bar{u}_\theta - \bar{u}_z$ 为热成风偏差, 则波包能量方程可写成:

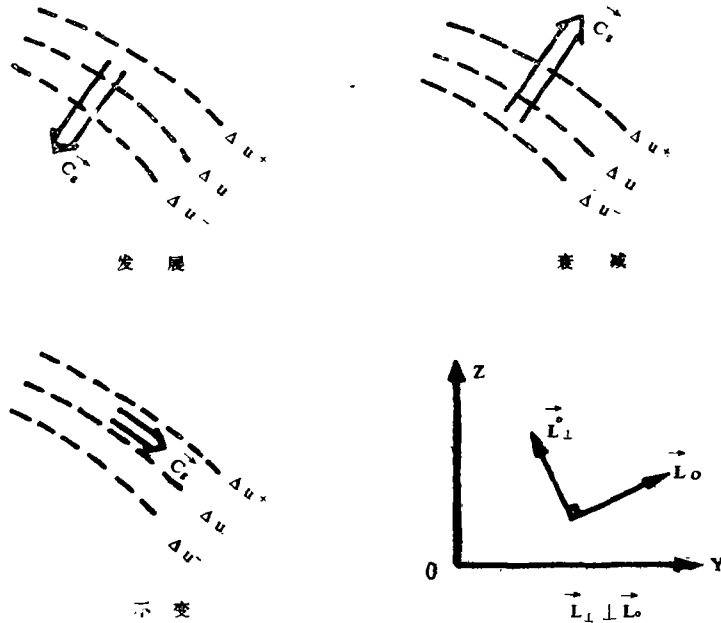
$$\begin{aligned} \frac{\partial E}{\partial T} &= \iint_{\sigma} \frac{f A_0^2}{2\omega} \left[k \frac{\partial \Delta \bar{u}_\theta}{\partial Z} - n \frac{\partial \Delta \bar{u}_\theta}{\partial Y} \right] dY dZ \\ &= - \iint_{\sigma} \frac{f \gamma^2 A_0^2}{2\omega} [\mathbf{I}_\perp^0 \cdot \nabla(\Delta \bar{u}_\theta)] dY dZ \end{aligned} \quad (31)$$

其中 \mathbf{I}_\perp^0 定义同前。通过简单地验证可以证明 \mathbf{I}_\perp^0 即是与群速度 \mathbf{C}_g 的方向平行的单位矢量, 即

$$\mathbf{I}_\perp^0 = \mathbf{C}_g / |\mathbf{C}_g| \quad (32)$$

由(31)式我们可以分析定常大尺度基流的热成风偏差所造成的扰动波包的对称发展问题。

扰动波包是否对称发展完全由此波包区域中热成风偏差的分布所决定。如果热成风偏差的梯度与 \mathbf{C}_g 的方向, 即波包(能量)传播方向不垂直, 也可以说等热成风偏差线不与波包传播方向一致, 则扰动波包可能对称发展。当热成风偏差的梯度与 \mathbf{C}_g 的方向一致时, 扰动波包对称发展最强; 反之, 若热成风偏差的梯度方向与 \mathbf{C}_g 方向相反时, 对称衰减最快。由此我们可以归纳出扰动波包对称发展与衰减的模型如下图:



由于重力惯性波是双向传播的, 所以, 当一个方向的波对称发展时, 另一个方向的波

一定对称衰减。

扰动波包对称发展与否决定于基本场的热成风偏差的分布,所以,对称发展过程是与基本场的热成风适应过程相联系的。扰动波包对称发展从基本场获得能量,从而消除这种热成风偏差和其不均匀性,最终使之达到热成风平衡,扰动也就不再发展。实际大气也正是处在这样一种扰动与基本场相互依存,相反相成的动态平衡之中。

五、主要结论

综上所述,我们可以把所获得主要结论归纳如下:

1. 如果基本场是定常的且满足热成风平衡,则扰动波包能量守恒。
2. 如果基本场是热成风平衡的,但不定常,则扰动波包可能对称发展。如果 $\partial N^2/\partial T > 0$ 则对称发展的必要条件为

$$\left(\frac{\partial M^2}{\partial T}\right)^2 - \frac{\partial f f_a}{\partial T} \frac{\partial N^2}{\partial T} > 0$$

如果 $\partial N^2/\partial T < 0$, 则对称发展的充分条件为

$$\left(\frac{\partial M^2}{\partial T}\right)^2 - \frac{\partial f f_a}{\partial T} \frac{\partial N^2}{\partial T} < 0$$

3. 如果基本场定常,则扰动波包对称发展是和基本场的热成风偏差联系在一起的,是基本场的热成风适应过程。相对而言,前述热成风平衡时基本场不定常时扰动波包的对称发展则与基本场的演变过程联系在一起。

4. 双向传播的重力惯性波(包),如果一个方向扰动对称发展,则另一个方向传播的扰动必定对称衰减,而且这种发展和衰减在热成风偏差的梯度与波包传播方向 C_g 一致时最强。

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ON THE SYMMETRIC DEVELOPMENT OF MESOSCALE DISTURBANCES

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Abstract

The effects of baroclinic basic flow on a paralleled mesoscale disturbance development are researched. Using WKB method, the two dimensional perturbation equations with the non-momentum-divergence approximation are analyzed. The result indicates that the symmetric development of a mesoscale disturbance is due to the non-homogeneous thermal deviations and unstationality of the basic field.